

Efficiently Representing Thermal Processes in Urban Canopy Models



Climate Change Research Centre

Mathew Lipson (UNSW) – m.lipson@unsw.edu.au

Melissa Hart (UNSW), Marcus Thatcher (CSIRO), Andy Pitman (UNSW)

Never Stand Still



School of Biological Earth & Env. Science

Climate Change Research Centre



Background

Models participating in the last urban intercomparison project significantly under-represented storage heat flux - why?

We are revisiting typical parameterisations in an urban canyon model to try to reduce heat storage flux errors and allow the use of more realistic wall/roof parameters.





Conclusion: Interface scheme reduces heat storage errors compared with previous scheme, however storage still under represented, especially if using observed material parameters.

Lipson et al., 2016, Geoscientific Model Development Discussions (in review)

Part 2: Compare Aerodynamic Heat Transfer Parameterisations

Using the Australian Town (Thatcher & Hurley, 2012) ...

 q_{ext}

conduction (proposed)

 $q_{1,2}$

 $q_{2,3}$

 $q_{3,4}$

transfer schemes – the Jürges method

Cyclic Heat Capacity $(Jm^{-2}K^{-1})$

Half-laver: individual wall/roof ——— Half-laver: laver mean

Interface: individual wall/roof —•— Interface: laver mean

...and compare with a less common turbulent heat transfer scheme – the Harmon method (per Thatcher and Hurley, 2012).

Lavers

Half-layer MAE optimum: 10+ laye

🛧 Interface MAE optimum: 4 layers

Taylor Diagram – response of fluxes to parameterisations

6 12 18 Time (h)

 $24 \ 0$

 \rightarrow ΔQ_S : Interface mean

25th & 75th percent

12 Time (h)

18

6 12 Time (h)

— ΔQ_S: Observations mean

Obs: 25% - 75% range

18

 $24 \ 0$

 \rightarrow ΔQ_S : Half-layer mean

25th & 75th percentile

6 12 18 Time (h)



Conclusion: Harman scheme has overall best performance for this site, however groupings on Taylor diagram show material parameters and conduction scheme have bigger influence.

Part 3: Represent Internal Thermal Mass and Other Processes



- aTEB currently represents the building envelope only. As such, for lowest model errors, roofs and walls need unrealistically high heat capacities.
- We are now adding internal thermal processes including internal mass to assess whether we can improve this.
- As each process is added, we compare output to the EnergyPlus building energy modelling system (DOE, 2016).

- ✓ varying internal temperature (fully implicit) ✓ new conduction model (interface scheme)

Internal surface and air temperature response





Preliminary Conclusion: Work still underway – so far simple internal model compares well with stripped down EnergyPlus 8.6 model.

